macroworks



GLINT AND GLARE ASSESSMENT

Proposed Solar PV Energy Development.

Social Housing Bundle 4, Development on Collins Avenue, Whitehall, Dublin 9

Prepared by Macro Works Ltd.

July 2024

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1 INTRODUCTION

1.1.1 This Glint and Glare Assessment was carried out by Macro Works Ltd to determine the potential for solar reflectance effects upon aviation receptors in respect of proposed roof-mounted solar PV installations on the roof of a proposed residential development in located at the former Bring Centre, Collins Avenue, Whitehall, Co. Dublin. The proposed panels will be mounted on the top floor of the proposed development and will remain in a fixed position throughout the day and year (i.e. they will not rotate to track the movement of the sun). Figure 1 and Figure 2 refer. The aviation-based glint and glare assessment will assess the proposed panels at six tilt angles: 0 degrees, 5 degrees, 10 degrees, 15 degrees, 20 degree, and 25 degrees.



Figure 1: Aerial view indicating the approximate location of the proposed PV panels (yellow pin).



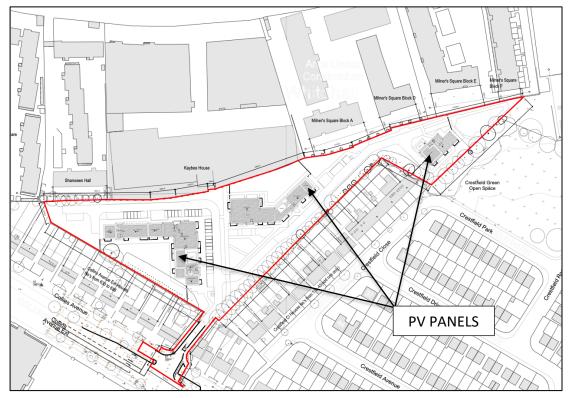


Figure 2: Extract showing the proposed roof layouts with the location of the proposed PV panels.

1.2 Project Description

- 1.2.1 Development at the site will consist of the following:
 - Development at the site will consist of the following:
 - The demolition of the existing office building, sheds, warehouses and garages and site clearance works.
 - Three apartment blocks comprising a total of 106 residential units and 375.3 sqm of community, arts and cultural space.
 - Block A ranges from 3 to 6 storeys and consists of 50 no. residential units (22 no. 1 bed, 20 no. 2 bed and 8 no. 3 bed units) and 272 sqm of community, arts and cultural facilities at ground floor level.
 - Block B ranges from 4 to 6 storeys and consists of 38 no. residential units (17 no. 1 bed, 9 no. 2 bed and 12 no. 3 bed units) and 99 sqm of community, arts and cultural facilities at ground floor level.
 - Block C ranges from 4 to 5 storeys and consists of 18 no. residential units (10 no. 1 bed and 8 no. 2 bed units).
 - 183 no. long-stay and 63 no. short-stay bicycle parking space, 57 no. car parking spaces and 5 no. motorcycle spaces.
 - 1,925 sqm of public open space and 3,140 sqm of communal open space.
 - One signalised vehicular access is proposed via Collins Avenue and Collins Avenue Extension.
 - Provision of pedestrian and cyclist access at northern boundary to allow for future link via Shanowen Business Estate and the Shanowen Hall and Square
 - Boundary treatments and planting, public lighting, site drainage works, internal road surfacing and footpath, ESB meter rooms, stores, bin and cycle storage, plant rooms, landscaping; and
 - All ancillary site services and development works above and below ground.



1.3 Statement of Authority

1.3.1 Macro Works' relevant experience includes twenty years of analysing the visual effects of a wide range of infrastructural and commercial development types. This experience includes numerous domestic and international wind and solar energy developments.

1.4 Guidance and Best Practice

- 1.4.1 Guidance has been prepared by the Federal Aviation Authority¹ to address the potential hazards that solar developments may pose to aviation activities, and this has been adopted for use by the Irish Aviation Authority. SGHAT was developed in conjunction with the FAA in harmony with this guidance and is commonly regarded as the accepted industry standard by aviation authorities internationally when considering the glint and glare effects upon aviation related receptors.
- 1.4.2 By virtue of their efficiency, the intensity of reflected light from modern PV solar panels is deliberately low and currently equates with that of the reflection from still water. Recent studies generally agree, however, that there still exists the potential for hazard or nuisance upon surrounding receptors. Macro Works' glint and glare analysis methods and determination of effects are based on a combination of available studies and established best practice. This methodology has been successfully implemented on numerous previous solar farm projects that met with the approval of both Planning Authorities and An Bord Pleanála.

Federal Aviation Authority

1.4.3 Within the FAA's interim policy, a 'Review of Solar Energy System Projects on Federally Obligated Airports'² it states:

"To obtain FAA approval to revise an airport layout plan to depict a solar installation and/or a "no objection" to a Notice of Proposed Construction Form 7460–1, the airport sponsor will be required to demonstrate that the proposed solar energy system meets the following standards:

No potential for glint or glare in the existing or planned Airport Traffic Control Tower (ATCT) cab, and

No potential for glare or "low potential for after-image" (shown in green in Figure 1 [Figure 3 refers]) along the final approach path for any existing landing threshold or future landing thresholds (including any planned interim phases of the landing thresholds) as shown on the current FAA-approved Airport Layout Plan (ALP). The final approach path is defined as two (2) miles from fifty (50) feet above the landing threshold using a standard three (3) degree glidepath."

1.4.4 Furthermore, in November 2021 the FAA deprioritised runway approaches as critical aviation receptors, citing the following;

"Initially, FAA believed that solar energy systems could introduce a novel glint and glare effect to pilots on final approach. FAA has subsequently concluded that in most cases, the glint and glare from solar energy systems to pilots on final approach is similar to glint and glare pilots routinely experience from water bodies, glass-façade buildings, parking lots, and similar features. However, FAA has continued to receive reports of potential glint and glare from on-airport solar energy systems on personnel working in ATCT cabs. Therefore, FAA has determined the scope of agency policy should be focused on the impact

¹ Harris, Miller, Miller & Hanson Inc. (November 2010). Technical Guidance for Evaluating Selected Solar Technologies on Airports; 3.1.2 Reflectivity. *Technical Guidance for Evaluating Selected Solar Technologies on Airports*. Available at: https://www.faa.gov/airports/environmental/policy_guidance/media/airport-solar-guide.pdf

² Federal Aviation Administration (FAA). (2013). Department of Transportation - Federal Aviation Administration. *Interim Policy, FAA Review of Solar Energy System Projects on Federally Obligated Airports*. Vol 78 (No 205), 63276-63279.



of on-airport solar energy systems to federally-obligated towered airports, specifically the airport's ATCT" (Federal Aviation Administration 05/11/2021).

1.4.5 In summary, glare at an ATCT is not acceptable and while still relevant glare with a "low potential for after-image" is generally acceptable along final approach paths to runways in most instances.

Solar Glare Hazard Analysis Tool

1.4.6 The SGHAT was designed to determine whether a proposed solar energy project would result in the potential for ocular impact as depicted on the Solar Glare Hazard Analysis Plot (Figure 3 refers). SGHAT analyses ocular impact over the entire calendar year in one minute intervals from when the sun rises above the horizon until the sun sets below the horizon. One of the principal outputs from the SGHAT report is a glare plot per receptor that indicates the time of day and days per year that glare has the potential to occur. SGHAT plot classifies the intensity of ocular impact as either Green Glare, Yellow Glare or Red Glare. These colour classifications are equivalent to the FAA's definitions regarding the level of ocular impact e.g. 'Green Glare' in the SGHAT is synonymous to the FAA's *"low potential for after-image',"* and so forth. The various correlations are illustrated on the Solar Glare Hazard Analysis Plot.

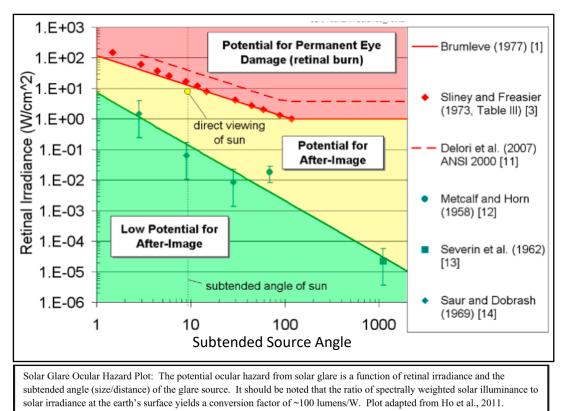


Chart References: Ho, C.K., C.M. Ghanbari, and R.B. Diver, 2011, Methodology to Assess Potential Glint and Glare Hazards from Concentrating Solar Power Plants: Analytical Models and Experimental Validation, J. Solar Energy Engineering, August 2011, Vol. 133, 031021-1 – 031021-9.

Figure 3: Figure 1 from the FAA Interim Policy, FAA Review of Solar Energy System Projects on Federally Obligated Airports

2 METHODOLOGY

- 2.1.1 The process for dealing with aviation receptors is as follows:
 - 1. The Federal Aviation Administration (FAA) approved Solar Glare Hazard Analysis Tool (SGHAT) is used to determine if any of these aviation receptors has the potential to theoretically experience glint or



glare. This tool also calculates the intensity of such reflectance and whether it is acceptable by FAA standards.

- 2. SGHAT does not account for terrain screening or screening provided by surface elements such as existing vegetation or buildings, therefore the results of the SGHAT may need to be considered, in conjunction with an assessment of existing intervening screening that may be present, to establish if reflectance can actually be experienced at the receptors.
- 3. Finally, if necessary, additional assessment is undertaken using Macro Works' bespoke model which would into account any screening provided by any proposed mitigation measures.

2.2 Identification of Relevant Receptors

2.2.1 The Planning and Development (Solar Safeguarding Zone) Regulations 2022 set out 43 Solar Safeguarding Zones (SSZs). A SSZ is an area around an airport, aerodrome or helipad in which there is a potential for glint or glare from solar panels to impact aviation safety.

Runways & Air Traffic Control Towers

2.2.2 This SGHAT analysis was produced to assess the potential for impacts upon aviation receptors, resulting from the proposed solar installation. Dublin Airport is located slightly over 4.5km to the north of the proposed development and comprises 3 active runways. Beaumont helipad is located just over 1.6km east of the site and is represented by 12 observation points.



Figure 4: Aerial view (Google Earth Pro) showing the approximate location of the proposed development (yellow pin) relative to the identified aviation receptors (red and green pins).

3 **RESULTS**

Runway Approaches – Dublin Airport



The SGHAT Optimisation results are contained in Appendix A and show that five of the six runway approaches analysed had potential for Green Glare to occur, depending on the panel tilt. Each of the panel areas was assessed at orientations of 175°, 180°, 185°, and tilts of 0°,5°, 10°, 15°, 20°, 25°. None of the six runways showed any potential for Yellow Glare as a result of the proposed solar panels. As a result, the 2-mile flight path approaches at Dublin Airport receive a 'pass' status as the flight path receptors do not receive yellow glare.

<u>Air Traffic Control Towers – Dublin Airport</u>

3.1.1 The SGHAT Optimisation results contained in Appendix A also assess the potential for reflectance at both of Dublin Airport Air Traffic Control Towers (ATCT) - Figure 5 below refers – with panel tilts of 0°,5°, 10°, 15°, 20°, 25°, and panel orientations of 175°, 180°, 185°. The assessment identifies no potential for reflectance from any of the proposed panel tilt angles at either ATCT at Dublin Airport. Thus, the assessment results in a 'pass' states as the ATCT receptors do not experience glare episodes as a result of the proposed development.

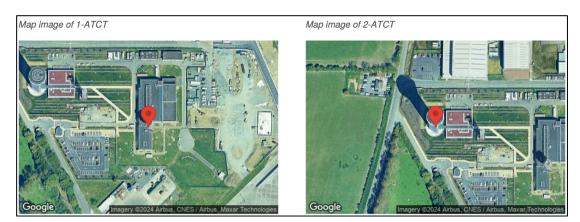


Figure 5: Aerial view (Google Earth Pro) showing the approximate location of the both Air Traffic Control Towers at Dublin Airport.

Observation Points – Beaumont Hospital

3.1.2 The SGHAT results show that each of the Observation Points analysed had potential for Green Glare to occur, depending on tilt and orientation. These are all low levels of glare , with none of the variations predicting as much as 700 minutes of green glare over the course of the year.

None of the Observation Points showed any potential for Yellow Glare as a result of the proposed solar panels. The absence of Yellow Glare is regarded as a pass in this assessment as there would only be low potential for after-image.

4 OVERALL CONCLUSION

4.1.1 From the analysis and discussions contained herein, it is considered that there will not be any significant nuisance effects from glint and glare at the proposed development, as a result of the proposed roof-mounted solar PV panels.



APPENDIX A

SGHAT Results



FORGESOLAR GLARE ANALYSIS

Project: Dublin North City

Site configuration: Social_Housing_Collins_Ave

Analysis conducted by Luis Dominguez (luis@macroworks.ie) at 09:27 on 18 Jul, 2024.

U.S. FAA 2013 Policy Adherence

The following table summarizes the policy adherence of the glare analysis based on the 2013 U.S. Federal Aviation Administration Interim Policy 78 FR 63276. This policy requires the following criteria be met for solar energy systems on airport property:

- No "yellow" glare (potential for after-image) for any flight path from threshold to 2 miles
- No glare of any kind for Air Traffic Control Tower(s) ("ATCT") at cab height.
- Default analysis and observer characteristics (see list below)

ForgeSolar does not represent or speak officially for the FAA and cannot approve or deny projects. Results are informational only.

COMPONENT	STATUS	DESCRIPTION
Analysis parameters	PASS	Analysis time interval and eye characteristics used are acceptable
2-mile flight path(s)	PASS	Flight path receptor(s) do not receive yellow glare
ATCT(s)	PASS	Receptor(s) marked as ATCT do not receive glare

Default glare analysis parameters and observer eye characteristics (for reference only):

- Analysis time interval: 1 minute
- Ocular transmission coefficient: 0.5
- Pupil diameter: 0.002 meters
- Eye focal length: 0.017 meters
- Sun subtended angle: 9.3 milliradians

FAA Policy 78 FR 63276 can be read at https://www.federalregister.gov/d/2013-24729



SITE CONFIGURATION

Analysis Parameters

DNI: peaks at 1,000.0 W/m^2 Time interval: 1 min Ocular transmission coefficient: 0.5 Pupil diameter: 0.002 m Eye focal length: 0.017 m Sun subtended angle: 9.3 mrad Site Config ID: 124494.19986 Methodology: V2



PV Array(s)

Name: Block A Axis tracking: Fixed (no rotation) Tilt: 10.0° Orientation: 178.0° Rated power: -Panel material: Smooth glass with AR coating Reflectivity: Vary with sun Slope error: correlate with material



Vertex	Latitude (°)	Longitude (°)	Ground elevation (m)	Height above ground (m)	Total elevation (m)
1	53.387257	-6.254845	48.00	13.80	61.80
2	53.387258	-6.254748	48.00	13.80	61.80
3	53.387151	-6.254746	48.00	13.80	61.80
4	53.387150	-6.254843	48.00	13.80	61.80
5	53.387257	-6.254845	48.00	13.80	61.80



Name: Block B Axis tracking: Fixed (no rotation) Tilt: 10.0° Orientation: 178.0° Rated power: -Panel material: Smooth glass with AR coating Reflectivity: Vary with sun Slope error: correlate with material



Vertex	Latitude (°)	Longitude (°)	Ground elevation (m)	Height above ground (m)	Total elevation (m)
1	53.387667	-6.253442	48.00	13.20	61.20
2	53.387624	-6.253372	48.00	13.20	61.20
3	53.387652	-6.253320	48.00	13.20	61.20
4	53.387700	-6.253393	48.00	13.20	61.20
5	53.387670	-6.253446	48.00	13.20	61.20

Name: Block C Axis tracking: Fixed (no rotation) Tilt: 10.0° Orientation: 135.0° Rated power: -Panel material: Smooth glass with AR coating Reflectivity: Vary with sun Slope error: correlate with material



Vertex	Latitude (°)	Longitude (°)	Ground elevation (m)	Height above ground (m)	Total elevation (m)
1	53.387867	-6.252098	47.50	15.90	63.40
2	53.387902	-6.252037	47.50	15.90	63.40
3	53.387886	-6.252012	47.50	15.90	63.40
4	53.387909	-6.251971	47.50	15.90	63.40
5	53.387858	-6.251890	47.50	15.90	63.40
6	53.387800	-6.251992	47.50	15.90	63.40
7	53.387850	-6.252069	47.50	15.90	63.40



Flight Path Receptor(s)

Name: 10L Runway
Description: None
Threshold height: 15 m
Direction: 95.8°
Glide slope: 3.0°
Pilot view restricted? Yes
Vertical view: 30.0°
Azimuthal view: 120.0°



Point	Latitude (°)	Longitude (°)	Ground elevation (m)	Height above ground (m)	Total elevation (m)
Threshold	53.436880	-6.280253	71.90	15.20	87.10
Two-mile	53.439822	-6.328592	74.90	180.90	255.80

Name: 10 Runway
Description: None
Threshold height: 15 m
Direction: 95.8°
Glide slope: 3.0°
Pilot view restricted? Yes
Vertical view: 30.0°
Azimuthal view: 120.0°



Point	Latitude (°)	Longitude (°)	Ground elevation (m)	Height above ground (m)	Total elevation (m)
Threshold	53.422405	-6.289520	74.00	15.30	89.30
Two-mile	53.425327	-6.337846	80.30	177.60	257.90

Name: 16 Runway Description: None Threshold height: 15 m Direction: 156.1° Glide slope: 3.0° Pilot view restricted? Yes Vertical view: 30.0° Azimuthal view: 120.0°		Google Tragery 62024 Arbus, Maxar Technologies			
Point	Latitude (°)	Longitude (°)	Ground elevation (m)	Height above ground (m)	Total elevation (m)
Threshold	53.436699	-6.261764	66.50	15.20	81.70
Two-mile	53.463138	-6.281428	69.70	180.70	250.40



Name: 28R Runway Description: None Threshold height: 15 m Direction: 275.9° Glide slope: 3.0° Pilot view restricted? Yes Vertical view: 30.0° Azimuthal view: 120.0°



Point	Latitude (°)	Longitude (°)	Ground elevation (m)	Height above ground (m)	Total elevation (m)
Threshold	53.435084	-6.240975	65.50	15.30	80.80
Two-mile	53.432097	-6.192645	34.00	215.50	249.50

Name: 28 Runway Description: None Threshold height: 15 m Direction: 275.5° Glide slope: 3.0° Pilot view restricted? Yes Vertical view: 30.0° Azimuthal view: 120.0°



Point	Latitude (°)	Longitude (°)	Ground elevation (m)	Height above ground (m)	Total elevation (m)
Threshold	53.420299	-6.251111	62.00	15.20	77.20
Two-mile	53.417517	-6.202763	41.90	204.00	245.90

Name: 34 Runway Description: None Threshold height: 15 m Direction: 336.6° Glide slope: 3.0° Pilot view restricted? Yes Vertical view: 30.0° Azimuthal view: 120.0°



Point	Latitude (°)	Longitude (°)	Ground elevation (m)	Height above ground (m)	Total elevation (m)
Threshold	53.420211	-6.249810	62.20	15.30	77.50
Two-mile	53.393680	-6.230504	49.00	197.10	246.10



Discrete Observation Receptors

Name	ID	Latitude (°)	Longitude (°)	Elevation (m)	Height (m)
1-ATCT	1	53.428489	-6.262201	65.90	21.90
2-ATCT	2	53.428937	-6.264259	65.60	75.60
OP 3	3	53.387892	-6.229964	47.40	1.70
OP 4	4	53.387892	-6.229964	47.40	25.00
OP 5	5	53.387892	-6.229964	47.40	50.00
OP 6	6	53.387892	-6.229964	47.40	75.00
OP 7	7	53.387892	-6.229964	47.40	100.00
OP 8	8	53.387892	-6.229964	47.40	125.00
OP 9	9	53.387892	-6.229964	47.40	150.00
OP 10	10	53.387892	-6.229964	47.40	175.00
OP 11	11	53.387892	-6.229964	47.40	200.00
OP 12	12	53.387892	-6.229964	47.40	225.00
OP 13	13	53.387892	-6.229964	47.40	250.00
OP 14	14	53.387892	-6.229964	47.40	275.00
OP 15	15	53.387892	-6.229964	47.40	300.00

Map image of 1-ATCT



Map image of 2-ATCT





Summary of Glare

PV Array Name	Tilt	Orient	"Green" Glare	"Yellow" Glare	Energy
	(°)	(°)	min	min	kWh
Block A	10.0	178.0	7,246	0	-
Block B	10.0	178.0	7,451	0	-
Block C	10.0	135.0	17,427	0	-

Total annual glare received by each receptor

Receptor	Annual Green Glare (min)	Annual Yellow Glare (min)
10L Runway	0	0
10 Runway	0	0
16 Runway	0	0
28R Runway	0	0
28 Runway	1578	0
34 Runway	6119	0
1-ATCT	0	0
2-ATCT	0	0
OP 3	395	0
OP 4	711	0
OP 5	1424	0
OP 6	1781	0
OP 7	2063	0
OP 8	2146	0
OP 9	2183	0
OP 10	2205	0
OP 11	2234	0
OP 12	2267	0
OP 13	2299	0
OP 14	2337	0
OP 15	2382	0



Results for: Block A

Receptor	Green Glare (min)	Yellow Glare (min)	
10L Runway	0	0	
10 Runway	0	0	
16 Runway	0	0	
28R Runway	0	0	
28 Runway	0	0	
34 Runway	164	0	
1-ATCT	0	0	
2-ATCT	0	0	
OP 3	0	0	
OP 4	109	0	
OP 5	405	0	
OP 6	521	0	
OP 7	613	0	
OP 8	671	0	
OP 9	679	0	
OP 10	677	0	
OP 11	679	0	
OP 12	683	0	
OP 13	681	0	
OP 14	681	0	
OP 15	683	0	

Flight Path: 10L Runway

0 minutes of yellow glare 0 minutes of green glare

Flight Path: 10 Runway

0 minutes of yellow glare 0 minutes of green glare

Flight Path: 16 Runway

0 minutes of yellow glare 0 minutes of green glare

Flight Path: 28R Runway

0 minutes of yellow glare 0 minutes of green glare

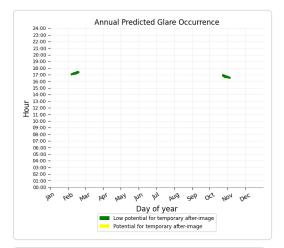


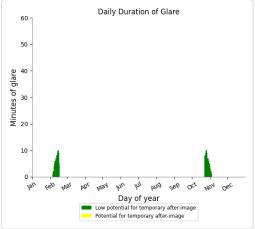
Flight Path: 28 Runway

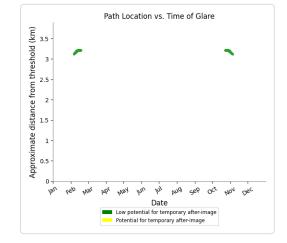
0 minutes of yellow glare 0 minutes of green glare

Flight Path: 34 Runway

0 minutes of yellow glare 164 minutes of green glare







Point Receptor: 1-ATCT

0 minutes of yellow glare 0 minutes of green glare

Point Receptor: 2-ATCT

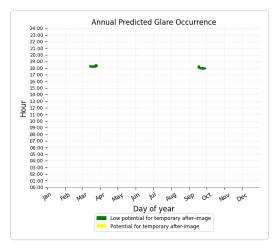
0 minutes of yellow glare 0 minutes of green glare

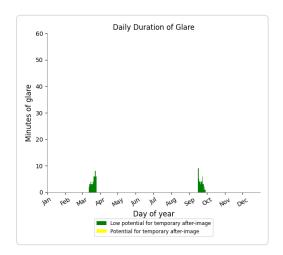
Point Receptor: OP 3

0 minutes of yellow glare 0 minutes of green glare



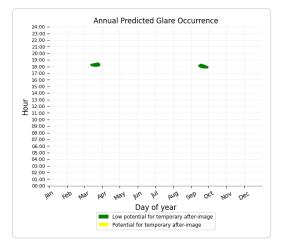
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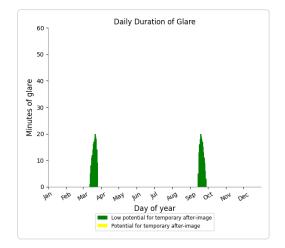




Point Receptor: OP 5

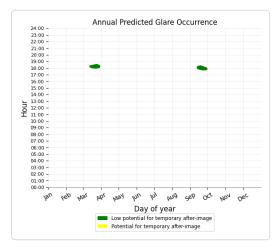
0 minutes of yellow glare 405 minutes of green glare

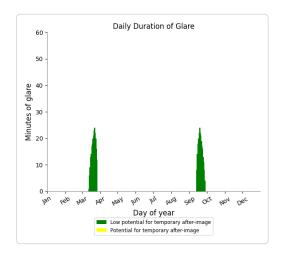






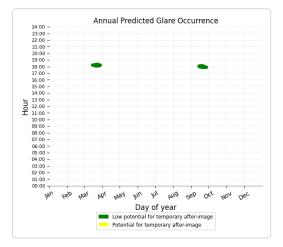
0 minutes of yellow glare 521 minutes of green glare

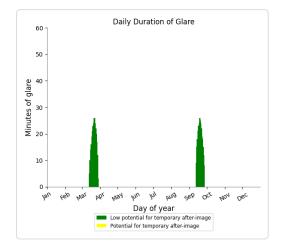




Point Receptor: OP 7

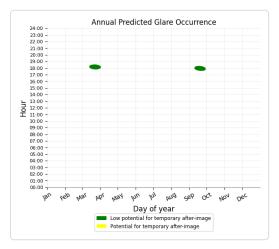
0 minutes of yellow glare 613 minutes of green glare

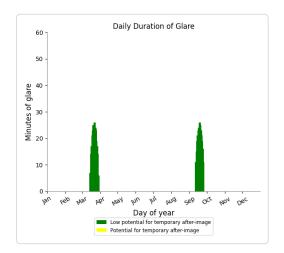






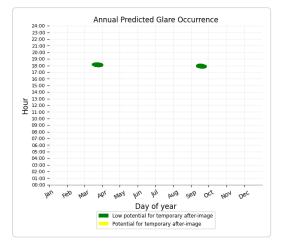
0 minutes of yellow glare 671 minutes of green glare

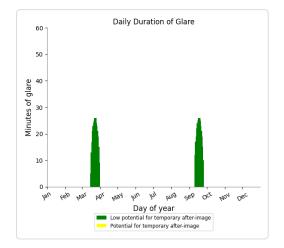




Point Receptor: OP 9

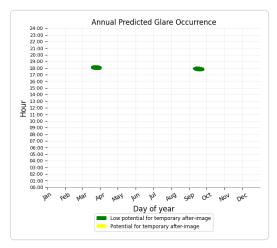
0 minutes of yellow glare 679 minutes of green glare

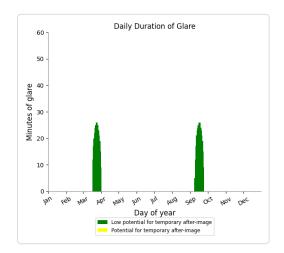






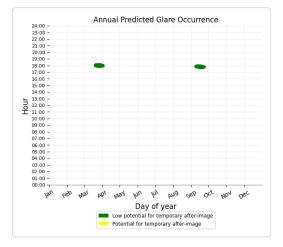
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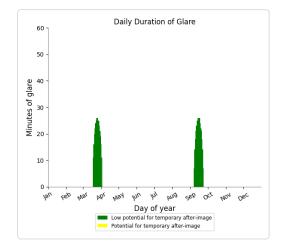




Point Receptor: OP 11

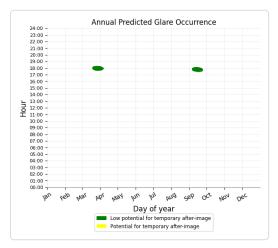
0 minutes of yellow glare 679 minutes of green glare

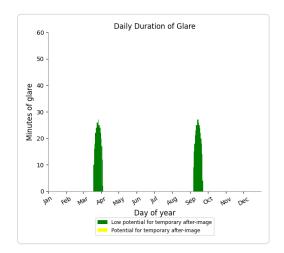






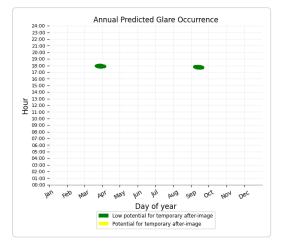
0 minutes of yellow glare 683 minutes of green glare

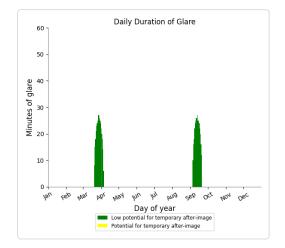




Point Receptor: OP 13

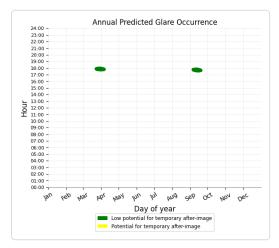
0 minutes of yellow glare 681 minutes of green glare

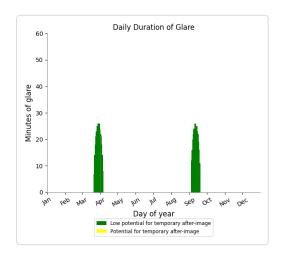






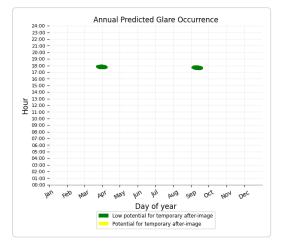
0 minutes of yellow glare 681 minutes of green glare

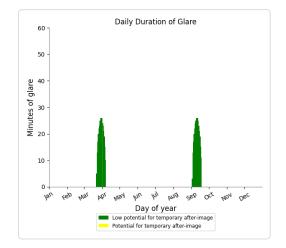




Point Receptor: OP 15

0 minutes of yellow glare 683 minutes of green glare







Results for: Block B

Receptor	Green Glare (min)	Yellow Glare (min)
10L Runway	0	0
10 Runway	0	0
16 Runway	0	0
28R Runway	0	0
28 Runway	0	0
34 Runway	258	0
1-ATCT	0	0
2-ATCT	0	0
OP 3	0	0
OP 4	232	0
OP 5	452	0
OP 6	553	0
OP 7	644	0
OP 8	655	0
OP 9	660	0
OP 10	662	0
OP 11	663	0
OP 12	662	0
OP 13	667	0
OP 14	669	0
OP 15	674	0

Flight Path: 10L Runway

0 minutes of yellow glare 0 minutes of green glare

Flight Path: 10 Runway

0 minutes of yellow glare 0 minutes of green glare

Flight Path: 16 Runway

0 minutes of yellow glare 0 minutes of green glare

Flight Path: 28R Runway

0 minutes of yellow glare 0 minutes of green glare

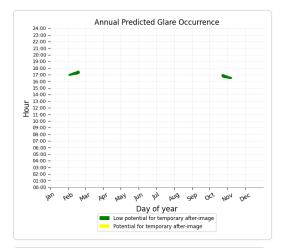


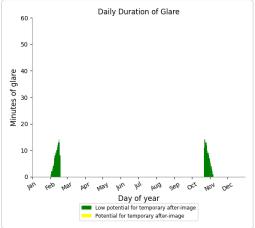
Flight Path: 28 Runway

0 minutes of yellow glare 0 minutes of green glare

Flight Path: 34 Runway

0 minutes of yellow glare 258 minutes of green glare





Point Receptor: 1-ATCT

0 minutes of yellow glare 0 minutes of green glare

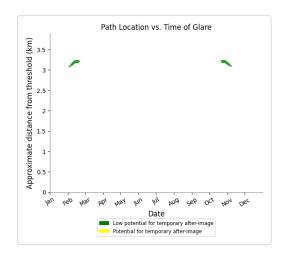
Point Receptor: 2-ATCT

0 minutes of yellow glare 0 minutes of green glare

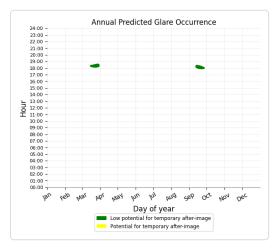
Point Receptor: OP 3

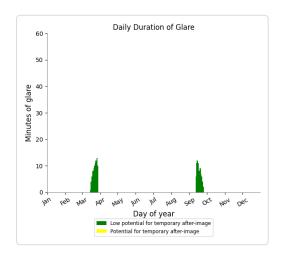
0 minutes of yellow glare 0 minutes of green glare





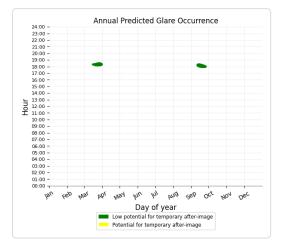
0 minutes of yellow glare 232 minutes of green glare

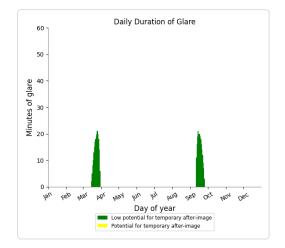




Point Receptor: OP 5

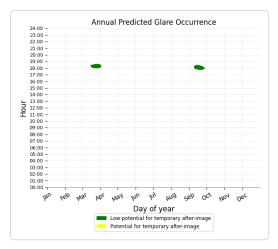
0 minutes of yellow glare 452 minutes of green glare

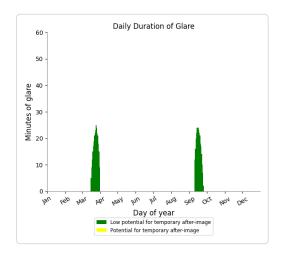






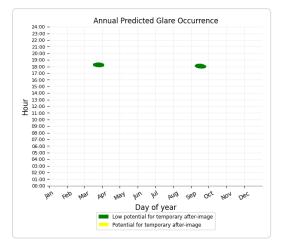
0 minutes of yellow glare 553 minutes of green glare

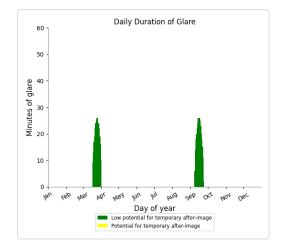




Point Receptor: OP 7

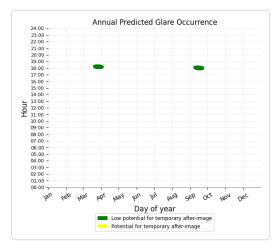
0 minutes of yellow glare 644 minutes of green glare

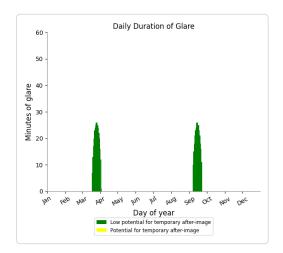






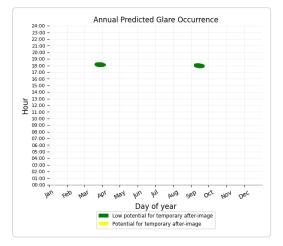
0 minutes of yellow glare 655 minutes of green glare

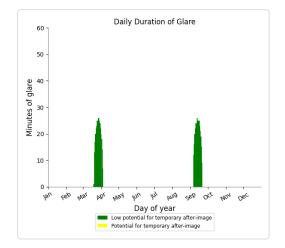




Point Receptor: OP 9

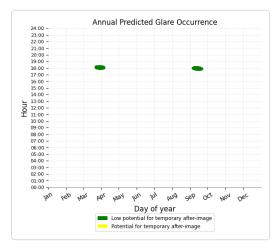
0 minutes of yellow glare 660 minutes of green glare

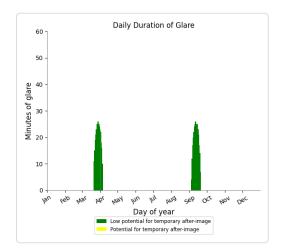






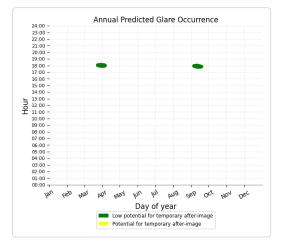
0 minutes of yellow glare 662 minutes of green glare

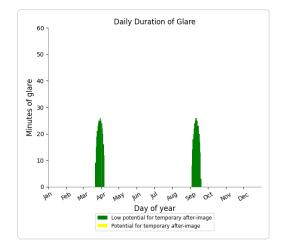




Point Receptor: OP 11

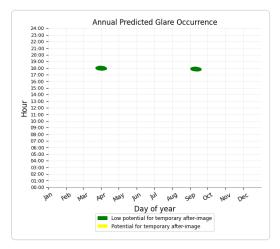
0 minutes of yellow glare 663 minutes of green glare

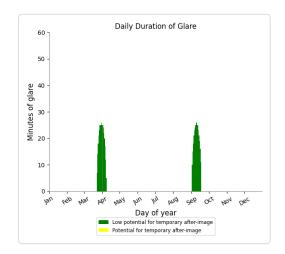






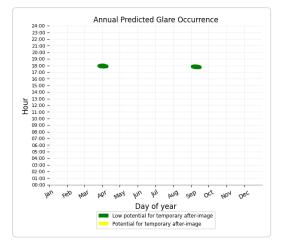
0 minutes of yellow glare 662 minutes of green glare

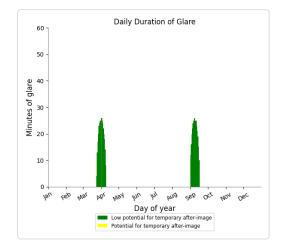




Point Receptor: OP 13

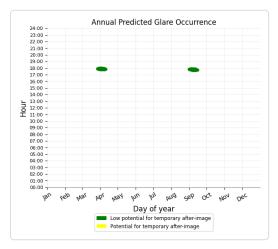
0 minutes of yellow glare 667 minutes of green glare

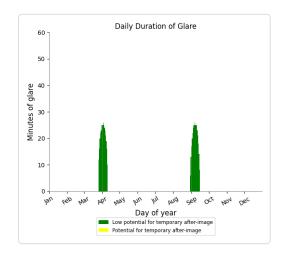






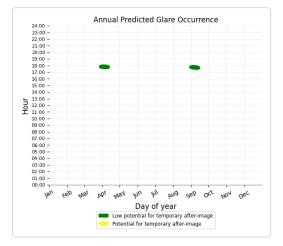
0 minutes of yellow glare 669 minutes of green glare

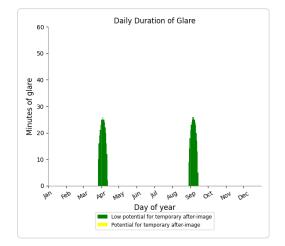




Point Receptor: OP 15

0 minutes of yellow glare 674 minutes of green glare







Results for: Block C

Receptor	Green Glare (min)	Yellow Glare (min)
10L Runway	0	0
10 Runway	0	0
16 Runway	0	0
28R Runway	0	0
28 Runway	1578	0
34 Runway	5697	0
1-ATCT	0	0
2-ATCT	0	0
OP 3	395	0
OP 4	370	0
OP 5	567	0
OP 6	707	0
OP 7	806	0
OP 8	820	0
OP 9	844	0
OP 10	866	0
OP 11	892	0
OP 12	922	0
OP 13	951	0
OP 14	987	0
OP 15	1025	0

Flight Path: 10L Runway

0 minutes of yellow glare 0 minutes of green glare

Flight Path: 10 Runway

0 minutes of yellow glare 0 minutes of green glare

Flight Path: 16 Runway

0 minutes of yellow glare 0 minutes of green glare

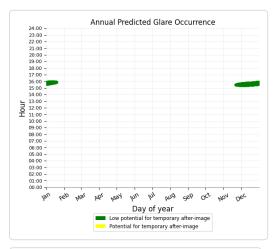
Flight Path: 28R Runway

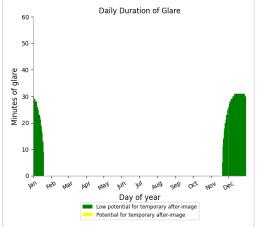
0 minutes of yellow glare 0 minutes of green glare

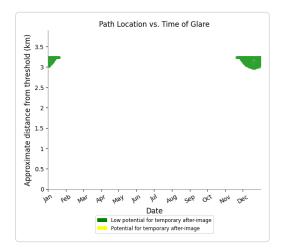


Flight Path: 28 Runway

0 minutes of yellow glare 1578 minutes of green glare



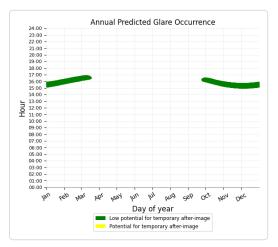


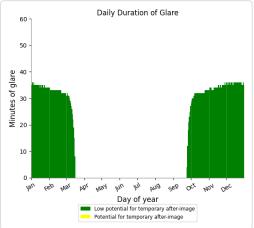




Flight Path: 34 Runway

0 minutes of yellow glare 5697 minutes of green glare



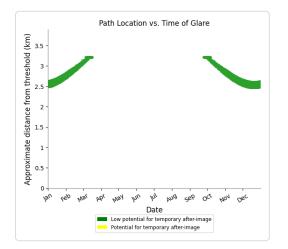


Point Receptor: 1-ATCT

0 minutes of yellow glare 0 minutes of green glare

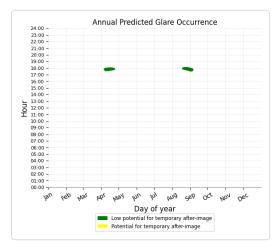
Point Receptor: 2-ATCT

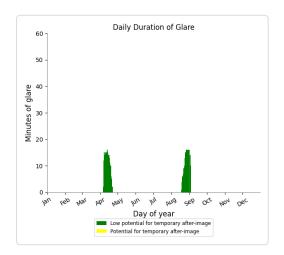
0 minutes of yellow glare 0 minutes of green glare





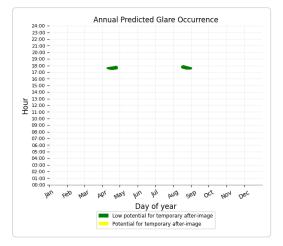
0 minutes of yellow glare 395 minutes of green glare

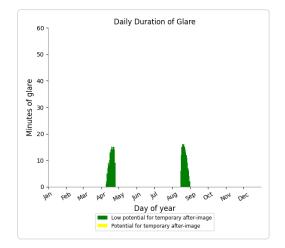




Point Receptor: OP 4

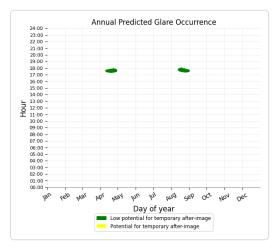
0 minutes of yellow glare 370 minutes of green glare

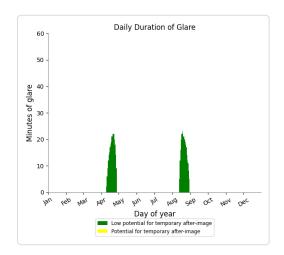






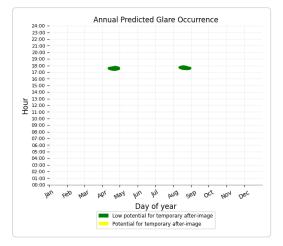
0 minutes of yellow glare 567 minutes of green glare

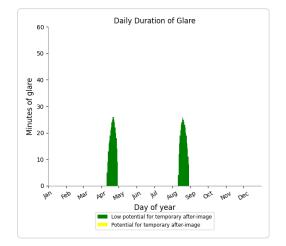




Point Receptor: OP 6

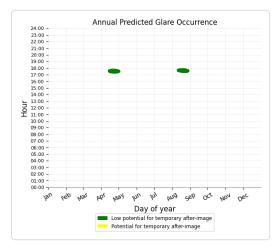
0 minutes of yellow glare 707 minutes of green glare

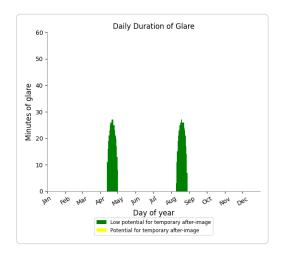






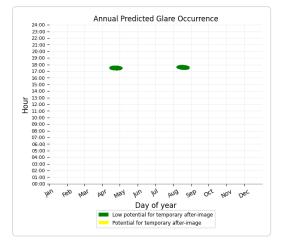
0 minutes of yellow glare 806 minutes of green glare

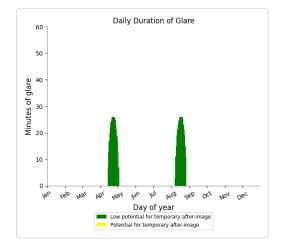




Point Receptor: OP 8

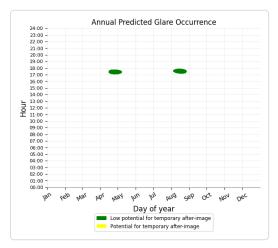
0 minutes of yellow glare 820 minutes of green glare

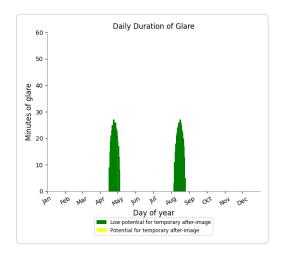






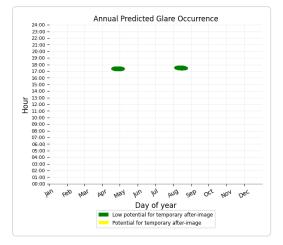
0 minutes of yellow glare 844 minutes of green glare

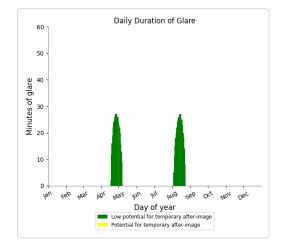




Point Receptor: OP 10

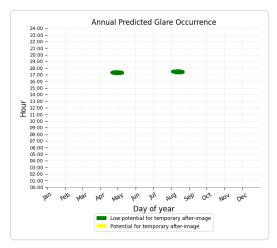
0 minutes of yellow glare 866 minutes of green glare

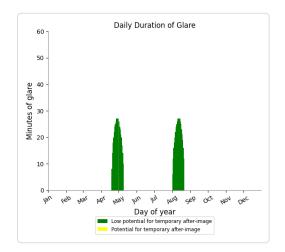






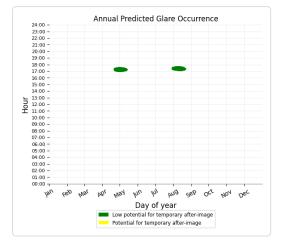
0 minutes of yellow glare 892 minutes of green glare

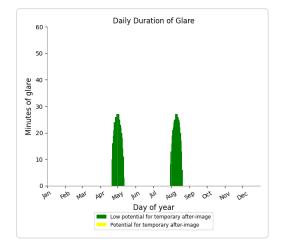




Point Receptor: OP 12

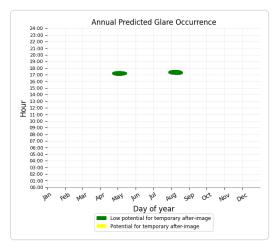
0 minutes of yellow glare 922 minutes of green glare

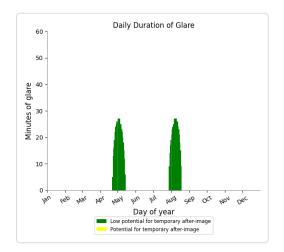






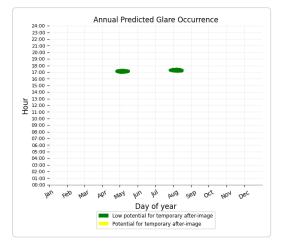
0 minutes of yellow glare 951 minutes of green glare

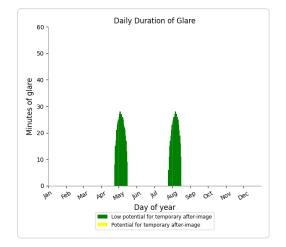




Point Receptor: OP 14

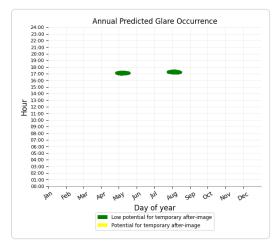
0 minutes of yellow glare 987 minutes of green glare

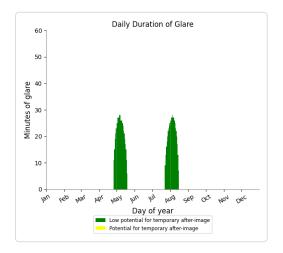






0 minutes of yellow glare 1025 minutes of green glare





Assumptions

"Green" glare is glare with low potential to cause an after-image (flash blindness) when observed prior to a typical blink response time. "Yellow" glare is glare with potential to cause an after-image (flash blindness) when observed prior to a typical blink response time. Times associated with glare are denoted in Standard time. For Daylight Savings, add one hour.

Glare analyses do not account for physical obstructions between reflectors and receptors. This includes buildings, tree cover and geographic obstructions.

Several calculations utilize the PV array centroid, rather than the actual glare spot location, due to V1 algorithm limitations. This may affect results for large PV footprints. Additional analyses of array sub-sections can provide additional information on expected glare. The subtended source angle (glare spot size) is constrained by the PV array footprint size. Partitioning large arrays into smaller sections will reduce the maximum potential subtended angle, potentially impacting results if actual glare spots are larger than the sub-array size. Additional analyses of the combined area of adjacent sub-arrays can provide more information on potential glare hazards. (See previous point on related limitations.)

Glare locations displayed on receptor plots are approximate. Actual glare-spot locations may differ.

Glare vector plots are simplified representations of analysis data. Actual glare emanations and results may differ.

The glare hazard determination relies on several approximations including observer eye characteristics, angle of view, and typical blink response time. Actual results and glare occurrence may differ.

Hazard zone boundaries shown in the Glare Hazard plot are an approximation and visual aid based on aggregated research data. Actual ocular impact outcomes encompass a continuous, not discrete, spectrum.

Refer to the Help page at www.forgesolar.com/help/ for assumptions and limitations not listed here.

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Optimization Results

ForgeSolar

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Projects / Project info / Optimizations / Block A

Block A

PV configurations in optimization: 18 Orientation (deg) range: 175 to 185 in intervals of 5 Titt angle (deg) range: 0 to 25 in intervals of 5 Creates: July 18, 2024 549 a.m. Completed: July 18, 2024 5:50 a.m.

Flight path receptors: 6 Route receptors: 0 Observation point receptors: 15 ATCT-specific OP receptors: 2

Note: OPs must be marked as "ATCT" to be included in FAA summary

FAA 2013 Policy Summary Table

Passifail results of each optimization case pertaining to FAA policy. Percentages denote system output relative to theoretical max. Blue, adheres to FAA policy (no glare for ATCT, only green for flight paths). Red: Fails FAA policy

Tilt → Orient ↓	0°	5°	10°	15°	20°	25°
175°	-	-	-	-	-	-
180°	-	-	-	-	-	-
185°	-	-	-	-	-	-

Color-Coded Hazard Summary Table

Results of each optimization case colored by maximum hazard. Percentages denote system output relative to theoretical max. Yeliow: glare with low potential for after-image found. Green: glare with low potential for after-image. Blue: no glare found.

 Blue: no glare found:

 Tilt → Orient ↓
 0°
 5°
 10°
 15°
 20°
 25°

 175°

180°	-	-	-	-	-	
185°	-	-	-	-	-	

2-Mile Flight Path Glare

Case results summary for FP receptors only.

Tilt → Orient ↓	0°	5°	10°	15°	20°	25°
175°	-	-	-	-	-	-
180°	-	-	-	-	-	-
185°	-	-	-	-	-	-

Observation Point Glare

Case results summary for OP receptors, including ATCTs.

Tilt → Orient ↓	0°	5°	10°	15°	20°	25°
175°	-	-	-	-	-	-
180°	-	-		-	-	-
185°	-	-	-	-	-	-

ATCT Glare

Case results summary for ATCT receptor(s) only.

Tilt → Orient ↓	0°	5°	10°	15°	20°	25°
175°	-	•	-	-	-	-
180°	-	-		-	-	-
185°	-	-	-	-	-	-

Glare & Energy Summary

Compilation of results for each PV configuration. Hazard, minutes of glare and energy produced.

Panel Orientation	Panel Tilt	"Green" Glare	"Yellow" Glare	"Red" Glare	Energy Produced	% Max Energy
deg	deg	min	min	min	kWh	% of max
175.0	5.0	10,459	0	0	-	-
175.0	15.0	7,378	0	0	-	-
175.0	20.0	7,358	0	0		-
175.0	0.0	20,817	0	0	-	-
180.0	0.0	20,817	0	0	-	-
175.0	25.0	7,353	0	0	-	÷

175.0	10.0	7,797	0	0	-	-
180.0	5.0	9,414	0	0	-	-
180.0	10.0	6,798	0	0	-	-
180.0	15.0	6,404	0	0	-	-
180.0	20.0	5,924	0	0	-	-
180.0	25.0	5,219	0	0	-	-
185.0	0.0	20,817	0	0	-	-
185.0	5.0	8,449	0	0	-	-
185.0	10.0	5,663	0	0	-	-
185.0	15.0	4,483	0	0	-	-
185.0	20.0	3,060	0	0	-	-
185.0	25.0	1,418	0	0	-	-

Results Per Component

PV		% Max	101-	10-	16-	28r-	28-	34-	1-	2-								OP	OP	OP	OP	OP	OP
Orientation	Tilt	Energy	ru	run	run	ru	run	run	ATCT	ATCT	OP 3	OP 4	OP 5	OP 6	OP 7	OP 8	OP 9	10	11	12	13	14	15
175.0	5.0	-	-	-	-	-	-	3,018	-	-	-	303	455	560	648	671	680	676	681	683	691	693	700
								green				green	gree										
175.0	15.0	-	-	-	-	-	-	-	-	-	-	286	456	566	653	674	678	679	680	673	677	677	679
												green	gree										
175.0	20.0	-	-	-	-	-	-	-	-	-	-	274 green	461 green	567 green	656 green	672 green	672 green	678 green	677 green	673 green	680 green	676 green	672 gree
175.0	0.0		457	2.953	-	429	2.516	7.087	-	_	-	270	427	541	628	673	678	680	683	693	695	701	706
110.0	0.0		green	green		green	green	green				green	gree										
180.0	0.0		457	2,953		429	2,516	7,087	-	-	-	270	427	541	628	673	678	680	683	693	695	701	706
			green	green		green	green	green				green	gree										
175.0	25.0	-	-	-	-	-	-	-	-	-	38	257	459	570	649	669	673	676	673	674	672	673	670
											green	green	green	green	green	green	green	green	green	green	green	green	gree
175.0	10.0	-	-	-	-	-	-	373	-	-	-	298	457	571	651	675	675	675	679	680	687	686	690
								green				green	gree										
180.0	5.0	-	-	-	-	-	-	2,400	-	-	-	54	390	515	609	667	674	673	680	684	685	691	692
								green				green	gree										
180.0	10.0	-	-	-	-	-	-	63	-	-	-	-	323	463	563	646	673	672	673	679	678	682	683
400.0	15.0							green					green	gree									
180.0	15.0	-	-	-	-	-	-	-	-	-	-	-	237 green	392 green	494 green	585 green	652 green	674 green	678 green	671 green	673 green	672 green	676 gree
180.0	20.0		-										108	323	408	495	578	632	674	679	675	676	676
100.0	20.0												green	gree									
180.0	25.0		-		-	-	-	-	-	-	-	-	-	242	324	394	465	530	589	641	674	683	677
														green	gree								
185.0	0.0	-	457	2,953	-	429	2,516	7,087	-	-	-	270	427	541	628	673	678	680	683	693	695	701	706
			green	green		green	green	green				green	gree										
185.0	5.0	-	-	-	-	-	-	1,809	-	-	-	-	277	432	540	631	673	678	676	685	678	688	682
								green					green	gree									
185.0	10.0	-	-	-	-	-	-	-	-	-	-	-	-	251	358	464	564	643	672	678	678	676	679
														green	gree								
185.0	15.0	-	-	-	-	-	-	-	-	-	-	-	-	-	175	267	373	467	561	630	673	672	665
105.0															green	gree							
185.0	20.0	-	-	-	-	-	-	-	-	-	-	-	-	-	32 groon	93 areen	174 areen	254 areen	341 areen	429 groop	513 green	581 groop	643
															green	green	9	9	9	green	•	green	gree 405
185.0	25.0	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	25 groon	68 groop	130 groop	193 groop	262 groop	335 groop	
																	green	green	green	green	green	green	g

Other Settings

DNI: varies (1,000.0 W/m^2 peak) Ocular transmission coefficient: 0.5 Pupil diameter: 0.002 m Eye focal length: 0.017 m Sun subtended angle: 9.3 mrad

Analysis Methodology: Version 2 Enhanced subtended angle calculation: On

Assumptions

 Times associated with glare are denoted in Standard time. For Daylight Savings, add one hour.
 Glare analyses do not account for physical obstructions between reflectors and receptors. This includes buildings, tree cover and geographic obstructions.
 Detailed system geometry is not rigorously simulated.
 The glare hazard determination relies on several approximations including observer eye characteristics, angle of view, and typical blink response time. Actual values and results may vary.
 The system output calculations is a DN-based approximation that assumes clear, sumy skies year-round. It should not be used in place of more rigorous modeling methods.
 Several calculations utilize the PV array centroid, rather than the actual glare spot location, due to algorithm limitations. This may affect results for large PV footprints. Additional analyses of array sub-sections can provide additional information on expect Several calculations using the PV all any controls, failed using the exclusion of the combined area of adjacent sub-arrays can provide more information on protein any size. Additional analyses of the combined area of adjacent sub-arrays can provide more information on proteinal giare hazards. (See previous point on related limitations.)
Hazard zone bundaries shown in the Gare Hazard plot area approximation and visual and actual gaine spots are larger than the sub-array size. Additional analyses of the combined area of adjacent sub-arrays can provide more information on potential giare hazards. (See previous point on related limitations.)
Hazard zone bundaries shown in the Gare Hazard plot area approximation and visual aid. Actual outcomes encompass a continuous, not discrete, spectrum.
Gare vector plots are simplified representations of analysis data. Actual glare emanations and results may differ.
Refer to the Help page for assumptions and limitations not listed here.



Optimization Results

ForgeSolar

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Projects / Project info / Optimizations / Block B

Block B

PV configurations in optimization: 18 Orientation (deg) range: 175 to 185 in intervals of 5 Titt angle (deg) range: 0 to 25 in intervals of 5 Creates: July 18, 2024 549 a.m. Completed: July 18, 2024 5:51 a.m.

Flight path receptors: 6 Route receptors: 0 Observation point receptors: 15 ATCT-specific OP receptors: 2

Note: OPs must be marked as "ATCT" to be included in FAA summary

FAA 2013 Policy Summary Table

Passifail results of each optimization case pertaining to FAA policy. Percentages denote system output relative to theoretical max. Blue, adheres to FAA policy (no glare for ATCT, only green for flight paths). Red: Fails FAA policy

Tilt → Orient ↓	0°	5°	10°	15°	20°	25°
175°	-	-	-	-	-	-
180°	-	-	-	-	-	-
185°	-	-	1.	-	-	-

Color-Coded Hazard Summary Table

Results of each optimization case colored by maximum hazard. Percentages denote system output relative to theoretical max. Yeliow: glare with low potential for after-image found. Green: glare with low potential for after-image. Blue: no glare found.

 Blue: no glare found.

 Tilt → Orient ↓
 0°
 5°
 10°
 15°
 20°
 25°

 175°

180°	-	-	-	-	-	
185°	-	-	-	-	-	

2-Mile Flight Path Glare

Case results summary for FP receptors only.

Tilt → Orient ↓	0°	5°	10°	15°	20°	25°
175°	-	-	-	-	-	-
180°	-	-	-	-	-	-
185°	-	-	-	-	-	-

Observation Point Glare

Case results summary for OP receptors, including ATCTs.

Tilt → Orient ↓	0°	5°	10°	15°	20°	25°
175°	-	-	-	-	-	-
180°	-	-		-	-	-
185°	-	-	-	-	-	-

ATCT Glare

Case results summary for ATCT receptor(s) only.

Tilt → Orient ↓	0°	5°	10°	15°	20°	25°
175°	-	•	-	-	-	-
180°	-	-		-	-	-
185°	-	-	-	-	-	-

Glare & Energy Summary

Compilation of results for each PV configuration. Hazard, minutes of glare and energy produced.

Panel Orientation	Panel Tilt	"Green" Glare	"Yellow" Glare	"Red" Glare	Energy Produced	% Max Energy
deg	deg	min	min	min	kWh	% of max
175.0	0.0	20,993	0	0	-	
175.0	5.0	10,759	0	0	-	-
175.0	10.0	7,857	0	0	-	-
175.0	20.0	7,332	0	0	-	-
175.0	15.0	7,351	0	0	-	-
180.0	0.0	20,993	0	0	-	-

175.0	25.0	7,333	0	0	-	-
180.0	5.0	9,905	0	0	-	-
180.0	15.0	6,720	0	0	-	-
180.0	10.0	7,070	0	0	-	-
180.0	20.0	6,477	0	0	-	-
185.0	0.0	20,993	0	0	-	-
180.0	25.0	6,191	0	0	-	-
185.0	5.0	8,853	0	0	-	-
185.0	10.0	6,051	0	0	-	-
185.0	15.0	5,238	0	0	-	-
185.0	20.0	4,195	0	0	-	-
185.0	25.0	2,806	0	0	-	-

Results Per Component

PV		% Max	101-	10-	16-	28r-	28-	34-	1-	2-								OP	OP	OP	OP	OP	OP
Orientation	Tilt	Energy	ru	run	run	ru	run	run	ATCT	ATCT	OP 3	OP 4	OP 5	OP 6	OP 7	OP 8	OP 9	10	11	12	13	14	15
175.0	0.0	-	653	3,012	-	356	2,473	7,202	-	-		284	425	548	633	655	662	666	674	680	684	688	698
			green	green		green	green	green				green	gree										
175.0	5.0	-	-	-	-	-	-	3,362	-	-	-	324	462	577	651	658	664	661	669	678	678	685	690
175.0								green				green	gree										
175.0	10.0	-	-	-	-	-	-	493	-	-	-	327	467	579	655	656	665	661	667	669	670	674	674
175.0	20.0							green			55	green 321	green 469	green 578	green 646	green 650	green 657	green 657	green 658	green 662	green 658	green 663	gree 658
175.0	20.0	-	-	-	-	-	-	-	-	-	green	green	green	green	green	green	green	green	green	green	green	green	gree
175.0	15.0					-					19	319	470	580	654	659	657	659	665	661	671	671	666
110.0	10.0										green	green	green	green	green	green	green	green	green	green	green	green	gree
180.0	0.0	-	653	3,012		356	2,473	7,202	-	-	-	284	425	548	633	655	662	666	674	680	684	688	698
			green	green		green	green	green				green	gree										
175.0	25.0	-	-	-	-	-	-	-	-	-	84	316	463	576	651	653	657	657	653	655	664	654	650
											green	green	green	green	green	green	green	green	green	green	green	green	gree
180.0	5.0	-	-	-	-	-	-	2,750	-	-	-	223	412	535	625	656	662	665	667	672	673	682	683
								green				green	gree										
180.0	15.0	-	-	-	-	-	-	-	-	-	-	39	352	490	586	653	653	651	658	657	661	662	658
												green	gree										
180.0	10.0	-	-	-	-	-	-	131	-	-	-	120	389	521	617 areen	654	660 areen	659	662	660	667	664	666 gree
180.0	20.0							green				green	green 292	green 452	541	green 614	656	green 654	green 653	green 653	green 653	green 655	654
100.0	20.0			-		-			-	-		-	areen	green	gree								
185.0	0.0		653	3.012		356	2.473	7.202			-	284	425	548	633	655	662	666	674	680	684	688	698
			green	green		green	green	green				green	gree										
180.0	25.0	-	-	-	-	-	-	-	-	-		-	225	397	486	551	612	649	652	654	658	652	655
													green	gree									
185.0	5.0	-	-	-	-	-	-	2,152	-	-	-	-	322	477	582	649	656	661	664	668	669	674	679
								green					green	gree									
185.0	10.0	-	-	-	-	-	-	-	-	-	-	-	123	341	451	547	632	656	658	659	660	661	663
													green	gree									
185.0	15.0	-	-	-	-	-	-	-	-	-	-	-	-	188	297	400	492	581	648	662	651	659	660
														green	gree								
185.0	20.0	-	-	-	-	-	-	-	-	-	-	-	-	20 groop	156 groop	239 groop	329 groop	421 groop	503 groop	585 groop	636 groop	654 groop	652
405.0	05.0													green	gree								
185.0	25.0	-	-	-	-	-	-	-	-	-	-	-	-	-	42 green	94 green	165 green	234 green	310 green	383 green	465 green	526 green	587 gree

Other Settings

DNI: varies (1,000.0 W/m^2 peak) Ocular transmission coefficient: 0.5 Pupil diameter: 0.002 m Eye focal length: 0.017 m Sun subtended angle: 9.3 mrad

Analysis Methodology: Version 2 Enhanced subtended angle calculation: On

Assumptions

- Times associated with glare are denoted in Standard time. For Daylight Savings, add one hour.
 Glare analyses do not account for physical obstructions between reflectors and receptors. This includes buildings, tree cover and geographic obstructions.
 Detailed system geometry is not rigorously simulated.
 The glare hazard determination relies on several approximations including observer eye characteristics, angle of view, and typical blink response time. Actual values and results may vary.
 The system output calculations is a DN-based approximation that assumes clear, sumy skies year-round. It should not be used in place of more rigorous modeling methods.
 Several calculations utilize the PV array centroid, rather than the actual glare spot location, due to algorithm limitations. This may affect results for large PV footprints. Additional analyses of array sub-sections can provide additional information on expect Several calculations using the PV all any controls, failed using the exclusion of the combined area of adjacent sub-arrays can provide more information on protein any size. Additional analyses of the combined area of adjacent sub-arrays can provide more information on proteinal giare hazards. (See previous point on related limitations.)
 Hazard zone bundaries shown in the Gare Hazard plot area approximation and visual and actual gaine spots are larger than the sub-array size. Additional analyses of the combined area of adjacent sub-arrays can provide more information on potential giare hazards. (See previous point on related limitations.)
 Hazard zone bundaries shown in the Gare Hazard plot area approximation and visual aid. Actual outcomes encompass a continuous, not discrete, spectrum.
 Gare vector plots are simplified representations of analysis data. Actual glare emanations and results may differ.
 Refer to the Help page for assumptions and limitations not listed here.



Optimization Results

ForgeSolar

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Projects / Project info / Optimizations / Block C

Block C

PV configurations in optimization: 18 Orientation (deg) range: 175 to 185 in intervals of 5 Titt angle (deg) range: 0 to 25 in intervals of 5 Creates: July 18, 2024 550 am. Completed: July 18, 2024 5:52 am.

Flight path receptors: 6 Route receptors: 0 Observation point receptors: 15 ATCT-specific OP receptors: 2

Note: OPs must be marked as "ATCT" to be included in FAA summary

FAA 2013 Policy Summary Table

Passifail results of each optimization case pertaining to FAA policy. Percentages denote system output relative to theoretical max. Blue, adheres to FAA policy (no glare for ATCT, only green for flight paths). Red: Fails FAA policy

Tilt → Orient ↓	0°	5°	10°	15°	20°	25°
175°	-	-	-	-	-	-
180°	-	-	-	-	-	-
185°	-	-	-	-	-	-

Color-Coded Hazard Summary Table

Results of each optimization case colored by maximum hazard. Percentages denote system output relative to theoretical max. Yeliow: glare with low potential for after-image found. Green: glare with low potential for after-image. Blue: no glare found.

 Blue: no glare found.

 Tit → Orient ↓
 0°
 5°
 10°
 15°
 20°
 25°

 175°

180°	-	-	-	-	-	
185°	-	-	-	-	-	

2-Mile Flight Path Glare

Case results summary for FP receptors only.

Tilt → Orient ↓	0°	5°	10°	15°	20°	25°
175°	-	-	-	-	-	-
180°	-	-	-	-	-	-
185°	-	-	-	-	-	-

Observation Point Glare

Case results summary for OP receptors, including ATCTs.

Tilt → Orient ↓	0°	5°	10°	15°	20°	25°
175°	-	-	-	-	-	-
180°	-	-		-	-	-
185°	-	-	-	-	-	-

ATCT Glare

Case results summary for ATCT receptor(s) only.

Tilt → Orient ↓	0°	5°	10°	15°	20°	25°
175°	-	-	-	-	-	-
180°	-	-	-	-	-	-
185°	-	-	-	-	-	-

Glare & Energy Summary

Compilation of results for each PV configuration. Hazard, minutes of glare and energy produced.

Panel Orientation	Panel Tilt	"Green" Glare	"Yellow" Glare	"Red" Glare	Energy Produced	% Max Energy
deg	deg	min	min	min	kWh	% of max
175.0	0.0	21,215	0	0	-	
175.0	5.0	11,240	0	0	-	-
175.0	10.0	8,183	0	0	-	-
175.0	15.0	7,638	0	0	-	-
175.0	20.0	7,633	0	0	-	-
175.0	25.0	7,625	0	0	Ξ.	-

180.0	0.0	21,215	0	0	-	-
180.0	15.0	7,140	0	0	-	-
180.0	10.0	7,456	0	0	-	-
180.0	20.0	6,976	0	0	-	-
180.0	5.0	10,419	0	0	-	-
185.0	0.0	21,215	0	0	-	-
185.0	5.0	9,364	0	0	-	-
185.0	10.0	6,473	0	0	-	-
185.0	15.0	5,742	0	0	-	-
180.0	25.0	6,772	0	0	-	-
185.0	20.0	4,934	0	0	-	-
185.0	25.0	3,698	0	0	-	-

Results Per Component

PV		% Max	101-	10-	16-	28r-	28-	34-	1-	2-								OP	OP	OP	OP	OP	OF
Orientation	Tilt	Energy	ru	run	run	ru	run	run	ATCT	ATCT	OP 3	OP 4	OP 5	OP 6	OP 7	OP 8	OP 9	10	11	12	13	14	15
175.0	0.0	-	818	3,024	-	240	2,342	7,214	-	-	-	266	435	574	660	678	690	692	699	713	716	721	73
			green	green		green	green	green				green	gre										
175.0	5.0	-	-	-	-	-	-	3,555	-	-	-	309	474	602	678	683	687	690	698	704	711	721	72
175.0								green				green	gre										
175.0	10.0	-	-	-	-	-	-	536	-	-	-	317	477	603	681	680	685	691	694	701	704	704	71
175.0	15.0							green			47	green 316	green 480	green 601	green 679	green 670	green 680	green 686	green 692	green 693	green 694	green 698	gre 70
175.0	15.0	-	-	-	-	-	-	-	-	-	green	green	green	green	green	green	green	green	green	green	green	green	gre
175.0	20.0		-	-		-	-	-	-	-	95	309	478	606	682	676	677	684	681	685	684	690	68
											green	green	green	green	green	green	green	green	green	green	green	green	gre
175.0	25.0	-	-	-	-	-	-	-	-	-	138	312	475	600	678	675	677	675	685	682	678	676	67
											green	green	green	green	green	green	green	green	green	green	green	green	gre
180.0	0.0	-	818	3,024	-	240	2,342	7,214	-	-	-	266	435	574	660	678	690	692	699	713	716	721	73
			green	green		green	green	green				green	gre										
180.0	15.0	-	-	-	-	-	-	-	-	-	-	101	399	544	641	674	680	672	684	684	686	689	68
												green	gre										
180.0	10.0	-	-	-	-	-	-	153	-	-	-	161	420	562	656	673	679	686	684	692	697	695	69
400.0	00.0							green				green	gre										
180.0	20.0	-	-	-	-	-	-	-	-	-	-	76 green	366 green	511 green	613 green	670 green	678 green	675 green	673 green	682 green	680 green	675 green	67 gre
180.0	5.0	_		_	_	_	_	2,967	_	_	_	228	431	565	661	678	684	685	691	701	704	708	91e 71
100.0	0.0							green				green	gre										
185.0	0.0	-	818	3,024		240	2,342	7,214	-	-	-	266	435	574	660	678	690	692	699	713	716	721	73
			green	green		green	green	green				green	gre										
185.0	5.0	-	-	-	-	-	-	2,379	-	-	-	-	343	507	614	670	679	684	687	693	696	703	70
								green					green	gre									
185.0	10.0	-	-	-	-	-	-	-	-	-	-	-	176	396	511	607	677	678	680	682	687	686	69
													green	gre									
185.0	15.0	-	-	-	-	-	-	-	-	-	-	-	-	261	373	483	581	656	679	674	679	673	68
														green	gre								
180.0	25.0	-	-	-	-	-	-	-	-	-	-	51	318	471	572	636	668	670	678	684	677	675	67
405.0	00.0											green	gre										
185.0	20.0	-	-	-	-	-	-	-	-	-	-	-	-	130 green	238 areen	330 green	425 green	516 green	601 green	665 green	674 green	680 green	6 gre
195.0	25.0													green	9	•	•	•	•	-	-	-	-
185.0	25.0	-	-	-	-	-	-	-	-	-	-	-	-	-	111 green	181 green	260 green	341 green	425 green	507 green	575 green	628 green	6 gre

Other Settings

DNI: varies (1,000.0 W/m^2 peak) Ocular transmission coefficient: 0.5 Pupil diameter: 0.002 m Eye focal length: 0.017 m Sun subtended angle: 9.3 mrad

Analysis Methodology: Version 2 Enhanced subtended angle calculation: On

Assumptions

- Times associated with glare are denoted in Standard time. For Daylight Savings, add one hour.
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